

## 2. INSTRUMENTATION AND SAMPLE PREPARATION

analysing the size of the charge pulse produced, the energy of the photon is determined. The powder-diffraction pattern is recorded as a function of energy (typically somewhere within the range 10–150 keV, depending on the source) *via* a multichannel analyser (MCA). Instruments may have multiple detectors, at different  $2\theta$  angles covering different ranges in  $d$ -spacing (Barnes *et al.*, 1998), or arranged around a Debye–Scherrer ring, as in the 23-element semi-annular detector at beamline I12 at Diamond Light Source (Korsunsky *et al.*, 2010; Rowles *et al.*, 2012).

Prior to performing the EDD experiment, the detector and MCA system must be calibrated, *e.g.* by measuring signals from sources of known energy, such as  $^{241}\text{Am}$  (59.5412 keV) or  $^{57}\text{Co}$  (122.06014 and 136.4743 keV) at hard energies, and/or from the fluorescence lines of elements such as Mo, Ag, Ba *etc.* The  $2\theta$  angle also needs to be calibrated if accurate  $d$ -spacings are desired. This should be done by measuring the diffraction pattern of a standard sample with known  $d$  values.

The detector angle is typically chosen in the range  $2$ – $6^\circ$   $2\theta$  and influences the range of  $d$ -spacings accessible *via* the term  $1/\sin \theta$ , *i.e.* the lower the angle, the higher the energy needed to access any particular  $d$ . Normally, the range of most interest should be matched to the incident spectrum, taking account also of sample absorption and fluorescence, to produce peaks with high intensity. More than one detector at different angles can also be employed. Energy-sensitive Ge detectors do not count particularly fast, up to 50 kHz being a typical value compared to possibly 1–2 MHz with a scintillation detector. Hence they are relatively sensitive to pulse pile-up and other effects of high count rates (Cousins, 1994; Laundy & Collins, 2003; Honkimäki & Suortti, 2007), particularly if the synchrotron is operating in a mode with a few large electron bunches giving very intense pulses of X-rays on the sample.

The energy resolution of the detector is of the order of 2%, which dominates the overall resolution of the technique. Its main uses are where a fixed geometry with penetrating X-rays is required, *e.g.* in high-pressure cells, for *in situ* studies (Häusermann & Barnes, 1992), *e.g.* of chemical reactions under hydrothermal conditions (Walton & O'Hare, 2000; Evans *et al.*, 1995), electrochemistry (*e.g.* Scarlett *et al.*, 2009; Rijssenbeek *et al.*, 2011; Rowles *et al.*, 2012), or measurements of residual strain (Korsunsky *et al.*, 2010). Owing to the use of polychromatic radiation, the technique has very high flux on the sample and can be used for high-speed data collection, following rapid processes *in situ*. However, accurate modelling of the intensities of the powder-diffraction pattern for structural or phase analysis is difficult because of the need to take several energy-dependent effects into account, *e.g.* absorption and scattering factors, the incident X-ray spectrum, and the detector response. Nevertheless, examples where this has been successfully carried out have been published (*e.g.* Yamanaka & Ogata, 1991; Scarlett *et al.*, 2009).

A higher-resolution variant of the energy-dispersive technique can be performed by using a standard detector behind a collimator at fixed  $2\theta$  scanning the incident energy *via* the monochromator. The Hart–Parrish design with long parallel foils is suitable. Such an approach has been demonstrated in principle (Parrish, 1988), but is rarely used in practice. The advantage is to be able to measure data of improved  $d$ -spacing resolution, as compared to using an energy-dispersive detector, from sample environments with highly restricted access. In principle, as a further variant, white incident radiation could be used with scanning of  $\theta_a$ , the angle of the analyser crystal, and associated detector at  $2\theta_a$ , all at fixed  $2\theta$ .

## 2.2.5. Considerations for powder-diffraction experiments

Synchrotron radiation allows considerable flexibility for a powder-diffraction experiment, offering choice and optimization of a number of quantities such as the wavelength, with high energy resolution, range in  $d$ -spacing, angular resolution, angular accuracy, and spatial or time resolution (but not all of these can necessarily be optimized at the same time). Increasingly, powder-diffraction experiments at synchrotrons are combined with complementary measurements, simultaneously applying techniques such as Raman spectroscopy (Boccaleri *et al.*, 2007; Newton & van Beek, 2010), particularly when carrying out *in situ* studies of an evolving system. In this respect, the open nature of a synchrotron instrument, with space around the sample to position auxiliary equipment, is an advantage.

## 2.2.5.1. Polarization

Assuming the beam is 100% polarized in the horizontal plane of the synchrotron orbit and with detection in the vertical plane, there is no need for any polarization correction to the diffracted intensities. However, if a small amount of vertical polarization of the beam does need to be taken into account (possibly up to a few per cent depending on the source), the polarization factor that describes its effect on the intensity of the diffracted beam can be derived, following the approach of Azároff (1955) and Yao & Jinno (1982), as

$$P = \frac{1 - dp + dp \cos^2 2\theta \cos^2 2\theta_a}{1 - dp + dp \cos^2 2\theta_a} = \frac{1 - dp + dp \cos^2 2\theta \cos^2 2\theta_a}{1 - dp \sin^2 2\theta_a}, \quad (2.2.3)$$

where  $dp$  is the depolarization fraction (*i.e.* the fraction of the total intensity incident on the sample that is vertically polarized),  $2\theta_a$  is the Bragg angle of the analyser crystal (if any), and the denominator scales  $P$  to unity at  $2\theta$  equal to zero (Dwiggins, 1983) and is a constant for any particular experimental setup. If there is no analyser crystal, or we ignore the effect it would have (*i.e.* by putting  $2\theta_a = 0$ ), then

$$P = 1 - dp \sin^2 2\theta.$$

Beamline staff can usually advise on the appropriate values to use. These expressions reduce to the usual polarization factor for unpolarized ( $dp = 0.5$ ) laboratory X-rays without a monochromator or analyser crystal,  $\frac{1}{2}(1 + \cos^2 2\theta)$ .

An alternative formulation of equation (2.2.3) considers the ratio of the vertical to horizontal polarization,

$$rp = \frac{dp}{1 - dp} \quad \text{and} \quad dp = \frac{rp}{1 + rp},$$

so that

$$P = \frac{1 + rp \cos^2 2\theta \cos^2 2\theta_a}{1 + rp \cos^2 2\theta_a}. \quad (2.2.4)$$

Note that  $rp = 1.0$  for unpolarized (laboratory) X-rays. In reality, because the synchrotron beam is near 100% plane polarized,  $dp$  and  $rp$  have similar values. The same expressions can be used if diffracting and analysing in the horizontal plane, except that now the value of  $dp$  or  $rp$  is replaced with the value of  $(1 - dp)$  or  $1/rp$ , respectively.

For Debye–Scherrer rings detected on a 2D detector, the azimuthal angle around the ring needs to be taken into account, yielding

## 2.2. SYNCHROTRON RADIATION

$$P = (1 - dp)(\cos^2 2\theta \sin^2 \kappa + \cos^2 \kappa) + dp(\cos^2 2\theta \cos^2 \kappa + \sin^2 \kappa)$$

or

$$P = \frac{(\cos^2 2\theta \sin^2 \kappa + \cos^2 \kappa) + rp(\cos^2 2\theta \cos^2 \kappa + \sin^2 \kappa)}{1 + rp},$$

where  $\kappa$  is the azimuthal angle (zero in the vertical direction) (Rowles *et al.*, 2012).

### 2.2.5.2. Radiation damage

The intensity of the incident beam can be so high that radiation damage becomes a real concern, particularly for samples containing organic molecules, such as pharmaceuticals, or organometallic materials. Radiation damage manifests itself by progressive shifts (often anisotropic) in the peak positions, a general reduction in peak intensities and peak broadening as the sample's crystallinity degrades. With high-resolution data, the effects are easily seen and can appear after only a few seconds in the worst cases. In such circumstances it may be better to use a 1D or 2D PSD to collect data of sufficient statistical quality before the damage is too severe. However, if the highest-resolution data are required, *via* scanning an analyser crystal, then the problem can be alleviated by filling a long capillary with sample and translating it between scans to expose fresh sample to the beam, thus acquiring multiple data sets which can be summed together. Such an approach necessarily requires a sufficient amount of disposable sample. If attempting to study the evolution of a particular part of the sample, *e.g.* undergoing heat treatment in the beam, then substituting fresh sample is not necessarily an option, and radiation damage can be a frustrating hindrance.

### 2.2.5.3. Beam heating

With a photon intensity of the order  $10^{12}$  photons  $\text{mm}^{-2} \text{s}^{-1}$  incident on the sample – a possible value for the unfocused beam on a beamline based on an insertion device at a modern third-generation source – the power in the beam corresponds to a few  $\text{mW mm}^{-2}$ . If a small fraction is absorbed by the sample this can represent a significant heat load that becomes troublesome when trying to work with samples at cryogenic temperatures, where heat capacities are relatively low.

As an example, consider a sample of microcrystalline silicon, composed of cubic  $1 \mu\text{m}^3$  grains irradiated by a 31 keV beam (0.4 Å wavelength) with  $10^{12}$  photons  $\text{mm}^{-2} \text{s}^{-1}$ . The power of the beam is  $5 \text{ mW mm}^{-2}$  ( $31 \times 10^3 \text{ e} \times 10^{12} \text{ W mm}^{-2}$ ). The mass absorption coefficient of Si at 0.4 Å wavelength  $\mu/\rho \simeq 1.32 \text{ cm}^2 \text{ g}^{-1}$  (Milledge, 1968) leading to a linear absorption coefficient of  $3.1 \text{ cm}^{-1}$  (density of Si =  $2.33 \text{ g cm}^{-3}$ ). Any problems with absorption by such a sample might usually be discounted; for a 1-mm-diameter capillary the value of  $\mu r$  is 0.1, assuming the powder density is 2/3 of the theoretical density.

A single  $1\text{-}\mu\text{m}^3$  grain of cross section  $1 \mu\text{m}^2$  is hit by  $10^6$  photons  $\text{s}^{-1}$ , of which a small fraction are absorbed,

$$\begin{aligned} \text{photons absorbed} &= 10^6 [1 - \exp(-3.1 \times 10^{-4})] \\ &= 310 \text{ photons s}^{-1}, \end{aligned}$$

corresponding to an absorbed power of  $1.54 \times 10^{-12} \text{ W}$ . Not all this energy is retained; significant amounts are lost as fluorescence, Compton scatter *etc.* Consultation of tables of mass attenuation coefficients and mass energy-absorption coefficients (Hubbell, 1982; Seltzer, 1993) indicates that for Si at 31 keV about 80% of the energy is retained, thus a net heating power of

$1.2 \times 10^{-12} \text{ W}$ . The mass of the Si grain is  $2.33 \times 10^{-15} \text{ kg}$ . At ambient temperature, where the specific heat capacity of Si is  $704.6 \text{ J kg}^{-1} \text{ K}^{-1}$ , this leads to an instantaneous tendency to increase the temperature by  $\sim 0.7 \text{ K s}^{-1}$ . At cryogenic temperatures, *e.g.* 10 K, the specific heat capacity is over three orders of magnitude lower,  $0.28 \text{ J kg}^{-1} \text{ K}^{-1}$  (Desai, 1986), leading to a very strong tendency for the temperature to rise ( $1840 \text{ K s}^{-1}$ ). The extent of the potential problem varies depending on the real net absorption of energy of the sample at the wavelength being used. However, it is clear that to prevent local beam-heating effects, the absorbed energy must be removed from the sample as efficiently as possible, *i.e.* by having excellent thermal contact between the grains of the sample and the external medium. At cryogenic temperatures this can be accomplished *via* the He exchange gas in the cryostat. Thus, if using a capillary sample, the capillary must either be left unsealed, to allow the He to permeate between the grains of sample, or it must be sealed under He, allowing transport of the heat to the walls of the capillary. Sealing under air, nitrogen, argon or other atmosphere leads to a loss of heat-transport capability when the gas solidifies, with consequent unpredictable behaviour for the sample caused by the beam-heating effects. This can involve significant shifts in peak positions and peak broadening depending on the instantaneous local temperature gradients. The problems tend to be worse at softer energies, where X-ray absorption is generally higher. Notwithstanding the potential problems, good-quality low-temperature data can be measured with appropriate care.

### 2.2.5.4. Choice of wavelength

The tunability of synchrotron radiation allows the wavelength best suited to the measurements to be selected. The collimation of the beam from the source combined with a perfect crystal monochromator lead automatically to high energy resolution, with a narrow wavelength distribution about a mean value. Consequently there are no issues to contend with such as  $\alpha_1, \alpha_2$  doublets or other effects due to a composite incident spectrum, contributing to a relatively simple instrumental peak-shape function. High energy resolution is essential for high  $2\theta$  resolution, because, as shown in equation (2.2.1), the effect of the energy envelope is to broaden the diffraction peaks as  $2\theta$  increases.

In choosing the wavelength for an experiment, factors to consider include:

- The optimum operational range for the beamline to be used, which will principally depend on the characteristics of the source.
- Absorption: choosing a sufficiently hard energy generally reduces absorption and allows the use of a capillary specimen in transmission for a wide range of compounds, *e.g.* those containing transition metals or heavier elements, thus minimizing preferred orientation. Selecting the energy a little way below (in energy) the  $K$  or  $L_{\text{III}}$  absorption edge of an element in the sample may help minimize sample absorption. For any sample or series of samples, it is good practice in the planning of the experiment to calculate the linear absorption coefficient to assess the optimum capillary diameter, the wavelength to use and those to avoid.
- The use of hard energies can be advantageous for penetration through sample environments, although these should normally, as much as possible, be designed with appropriate X-ray windows *etc.* However, when absorbing environments are unavoidable, such as containing a sample in a spinning Pt