

## 3.4. INDEXING

**Table 3.4.1**

 Expressions for  $Q(hkl)$  for different types of symmetry

Symmetry	$Q(hkl)$
Cubic	$(h^2 + k^2 + l^2)A_{11}$
Tetragonal	$(h^2 + k^2)A_{11} + l^2A_{33}$
Hexagonal	$(h^2 + hk + k^2)A_{11} + l^2A_{33}$
Orthorhombic	$h^2A_{11} + k^2A_{22} + l^2A_{33}$
Monoclinic	$h^2A_{11} + k^2A_{22} + l^2A_{33} + hA_{13}$
Triclinic	$h^2A_{11} + k^2A_{22} + l^2A_{33} + hkA_{12} + hA_{13} + kA_{23}$

diffraction angles by

$$d_{hkl} = \lambda / (2 \sin \theta_{hkl}).$$

$d_{hkl}$ , the spacing of the planes ( $hkl$ ) in the direct lattice, is obtained by the dot products of the reciprocal-lattice vectors with themselves:

$$(\mathbf{r}_{hkl}^*)^2 = \frac{1}{d_{hkl}^2} = h^2 a^{*2} + k^2 b^{*2} + l^2 c^{*2} + 2hka^* b^* \cos \gamma^* + 2hla^* c^* \cos \beta^* + 2klb^* c^* \cos \alpha^*, \quad (3.4.1)$$

where  $\alpha^*$  is the angle between  $\mathbf{b}^*$  and  $\mathbf{c}^*$ ,  $\beta^*$  is the angle between  $\mathbf{c}^*$  and  $\mathbf{a}^*$ , and  $\gamma^*$  is the angle between  $\mathbf{a}^*$  and  $\mathbf{b}^*$ . If we introduce

$$Q(hkl) = \frac{10^4}{d_{hkl}^2}$$

[where  $Q(hkl)$  differs from  $\sin^2 \theta_{hkl}$  by a scale factor of  $(200/\lambda)^2$ ], (3.4.1) becomes

$$Q(hkl) = h^2 A_{11} + k^2 A_{22} + l^2 A_{33} + hkA_{12} + hA_{13} + kA_{23}, \quad (3.4.2)$$

where

$$\begin{aligned} A_{11} &= 10^4 a^{*2}, \quad A_{22} = 10^4 b^{*2}, \quad A_{33} = 10^4 c^{*2}, \\ A_{12} &= 2 \times 10^4 a^* b^* \cos \gamma^*, \quad A_{13} = 2 \times 10^4 a^* c^* \cos \beta^*, \\ A_{23} &= 2 \times 10^4 b^* c^* \cos \alpha^*. \end{aligned}$$

The number of parameters  $A_{ij}$  in (3.4.2) depends on the type of symmetry: from 1 in the case of cubic symmetry to 6 for triclinic symmetry (see Table 3.4.1).

The quadratic form (3.4.2) relates the observed  $Q(hkl)$  values to the reciprocal cell parameters and, consequently, to the direct cell. It is the basic equation used in powder-indexing procedures. Therefore the indexing problem (Werner, 2002) is to find  $A_{ij}$  and, for each observed  $Q(hkl)$  value, three crystallographic indices ( $hkl$ ) satisfying (3.4.2) within a suitable tolerance parameter  $\Delta$ :

$$Q(hkl) - \Delta < h^2 A_{11} + k^2 A_{22} + l^2 A_{33} + hkA_{12} + hA_{13} + kA_{23} < Q(hkl) + \Delta. \quad (3.4.3)$$

The importance of using accurate  $Q(hkl)$  values in (3.4.3) is obvious. Moreover, it is worth noticing that (3.4.3) must lead to physically reasonable indexing – low-angle peaks should correspond to small integer values for  $h$ ,  $k$  and  $l$  and the values of the cell parameters and cell volume should be reasonable.

## 3.4.2.1. Figures of merit

An important task is the introduction of a figure of merit (FOM) that is able to (a) describe the physical plausibility of a trial cell and its agreement with the observed pattern, and (b) select the best cell among different possible ones. de Wolff (1968) made an important contribution in this direction. He developed the  $M_{20}$  figure of merit defined by

$$M_{20} = \frac{Q_{20}}{2\langle \varepsilon \rangle N_{20}}, \quad (3.4.4)$$

where  $Q_{20}$  is the  $Q$  value corresponding to the 20th observed and indexed peak,  $N_{20}$  is the number of different calculated  $Q$  values up to  $Q_{20}$ , and  $\langle \varepsilon \rangle$  is the average absolute discrepancy between the observed and the calculated  $Q$  values for the 20 indexed peaks; the factor 2 is a result of statistics, explained by the larger chance for an observed line to sit in a large interval as compared with sitting in a small interval. The rationale behind  $M_{20}$  is as follows: the better the agreement between the calculated and the observed peak positions (the smaller the  $\langle \varepsilon \rangle$  value) and the smaller the volume of the unit cell (the smaller the  $N_{20}$  value), the larger the  $M_{20}$  value and consequently the confidence in the proposed unit cell. A rule of thumb for  $M_{20}$  is that if the number of unindexed peaks whose  $Q$  values are less than  $Q_{20}$  is not larger than 2 and if  $M_{20} > 10$ , then the indexing process is physically reasonable (de Wolff, 1968; Werner, 2002). This rule is often valid, but exceptions occur. The use of the first 20 peaks is a compromise (coming from experience) between introducing a quite large number of observed peaks (depending on the number of parameters of the unit cell) and avoiding the use of high-angle peak positions, which are more affected by errors.  $M_{20}$  is statistically expected to be 1 in case of completely arbitrary indexing. It has no upper limit (it can be very large when  $\langle \varepsilon \rangle$  is very small).

Smith & Snyder (1979) proposed the  $F_N$  criterion in order to overcome the limits of  $M_{20}$  with respect to its dependence on the 20 lines and on crystal class and space group. The  $F_N$  figure of merit is given by

$$F_N = \frac{1}{\langle |\Delta 2\theta| \rangle} \frac{N}{N_{\text{poss}}},$$

where  $\langle |\Delta 2\theta| \rangle$  is the average absolute discrepancy between the observed and calculated  $2\theta$  peak position values and  $N_{\text{poss}}$  is the number of possible diffraction lines up to the  $N$ th observed line. The values of  $\langle |\Delta 2\theta| \rangle$  and  $N_{\text{poss}}$ , ( $\langle |\Delta 2\theta| \rangle$ ,  $N_{\text{poss}}$ ), are usually given with  $F_N$ . With respect to  $M_{20}$ ,  $F_N$  is more suitable for ranking the trial solutions and less for indicating their physical plausibility (Werner, 2002).

Both  $M_{20}$  and  $F_N$ , being based on the discrepancies between observed and calculated lines, are less reliable if there are impurity peaks; if the information about the unindexed lines is not taken into account, the risk of obtaining false solutions increases. Alternative FOMs based on joint probability have also been proposed (Ishida & Watanabe, 1967, 1971). Among the recently developed FOMs, we mention:

 (1)  $Q_{\text{partial}}$  (Bergmann, 2007):

$$Q_{\text{partial}} = \sum_i \min \left[ w_i, \left( \frac{x_i - \hat{x}_i}{\delta_i} \right)^2 \right],$$

where the summation is over the number of observed lines,  $w_i$  is the observed weight of line  $i$ ,  $x$  and  $\hat{x}_i$  are the observed and simulated line positions, respectively, and  $\delta_i$  is the observed random error of line  $i$ .  $Q_{\text{partial}}$  is multiplied by a factor that depends on the symmetry of the simulated lattice (triclinic, ..., cubic), on the unit cell volume and on the number of ignored peaks.

 (2)  $McM_{20}$  (Le Bail, 2008):

$$McM_{20} = [100/(R_p N_{20})] B_r S_y,$$

where  $N_{20}$  is the number of possible lines that might exist up to the 20th observed line (for a primitive  $P$  lattice).  $R_p$  is